

ECE 3084

FINAL EXAM

SCHOOL OF ELECTRICAL AND COMPUTER ENGINEERING

GEORGIA INSTITUTE OF TECHNOLOGY

MAY 5, 2016

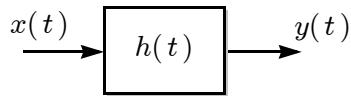
Name: \_\_\_\_\_

1. The exam is closed book, except for three 2-sided sheets of handwritten notes.
2. Turn off your phone and put it away. No tablets/laptops/WiFi/etc. Calculators are OK.
3. Final answers must be entered into the answer box.
4. Correct answers *must be accompanied by concise justifications* to receive full credit.
5. Do not attach additional sheets. If necessary, use the back of the previous page.

Problem	Points	Score
1	20	
2	15	
3	15	
4	15	
5	15	
6	20	
TOTAL:	100	

**PROBLEM 1.** (20 points)

Consider an LTI filter with a *rectangular* impulse response is  $h(t) = 4(u(t - 0.5) - u(t - 2.5))$ :



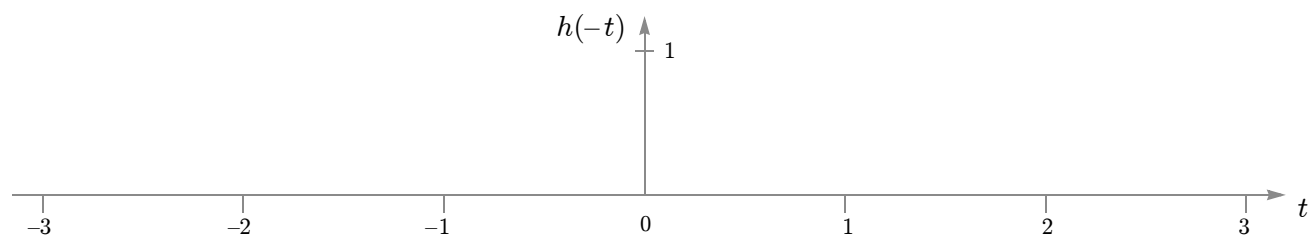
(a) The d.c. gain of the filter is  $H_0 =$   .

(b) The Laplace transform of  $h(t)$  is  $H(s) =$   .

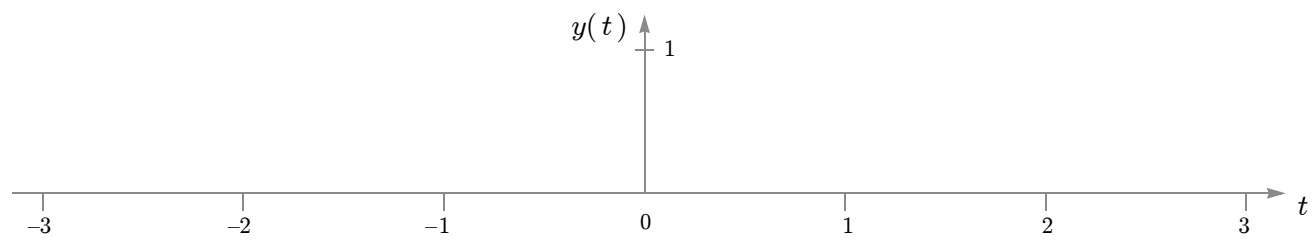
(c) Specify three values of  $f_0$  such that a sinusoidal input of the form  $x(t) = \cos(2\pi f_0 t)$  will result in a zero output:

$f_0 =$   , or  $f_0 =$   , or  $f_0 =$   .

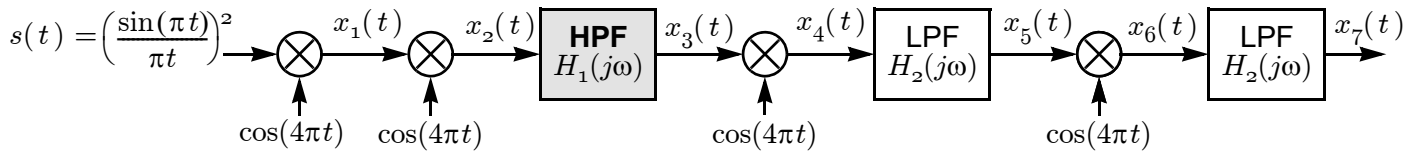
(d) Carefully sketch in the space below the signal  $h(-t)$ :



(e) Carefully sketch the output  $y(t)$  in the space below for the case when the input is  $x(t) = h(-t)$ :



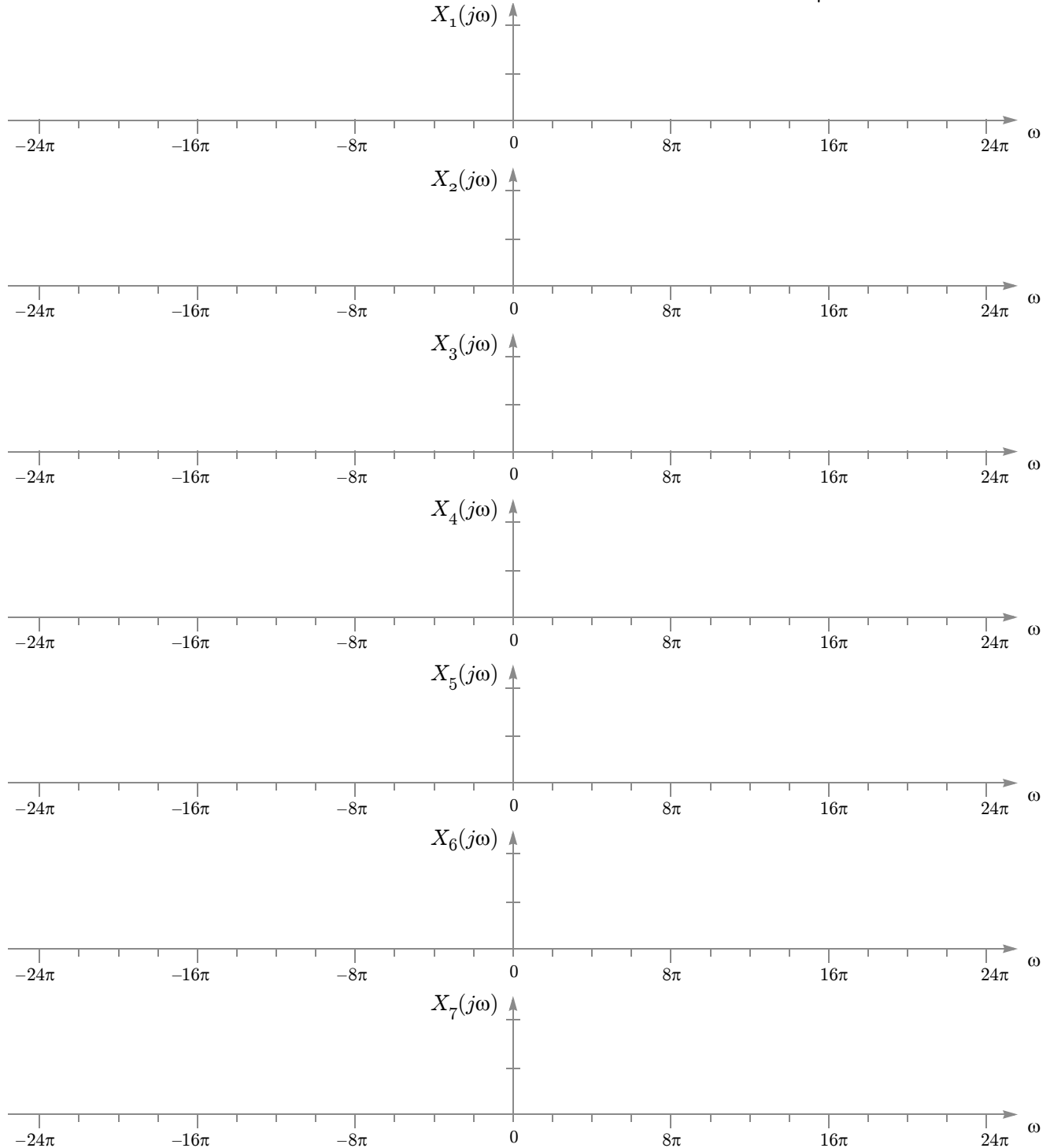
**PROBLEM 2.** Suppose  $s(t) = \left(\frac{\sin(\pi t)}{\pi t}\right)^2$  is fed into the following cascade of oscillators and filters:



The lone **HPF** is ideal with unity gain and rejects all frequencies below  $4\pi$  rad/s.

The two **LPF**'s are ideal with unity gain and reject all frequencies *above*  $4\pi$  rad/s.

Sketch in the space below the Fourier transform of each of the signals  $x_1(t)$  through  $x_7(t)$  in the diagram:



**PROBLEM 3.** (15 points)

Consider a 2nd-order system with transfer function

$$H(s) = \frac{1}{s^2 + bs + c},$$

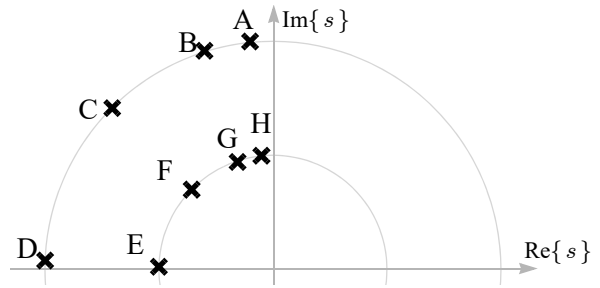
where the constants  $b$  and  $c$  are positive.

When  $b^2 < 4c$ , the two poles will be *complex*:

- one pole will be at a location  $p$  in the upper half of the  $s$  plane;
- the other pole will be at the conjugate location  $p^*$  in the lower half of the  $s$  plane.

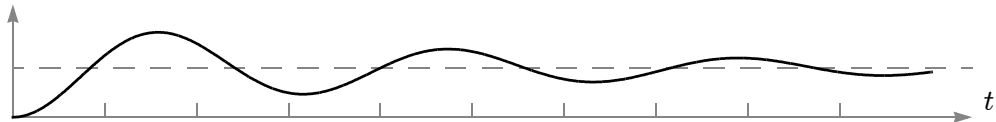
Shown above are eight possible locations for the upper pole  $p$ . (The lower pole at  $p^*$  is not shown.)

Match each location  $p$  above with its corresponding step response below by writing a letter from {A, B, C, D, E, F, G, H} into each answer box below:

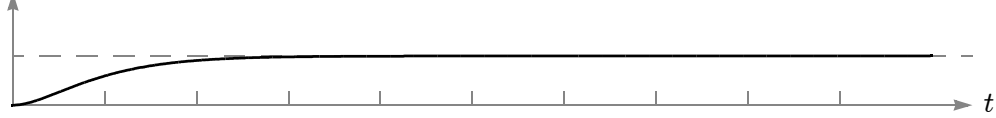


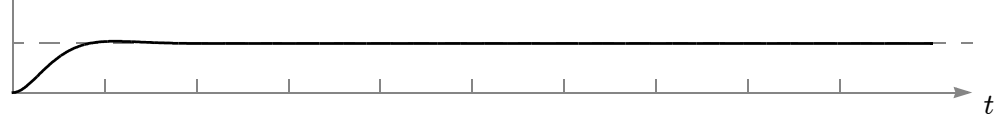
(a) .

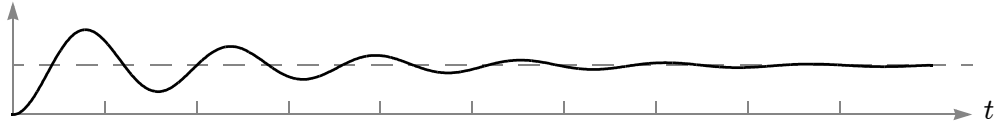


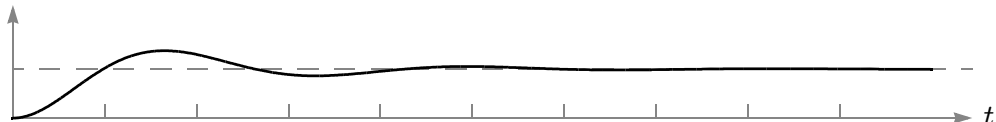






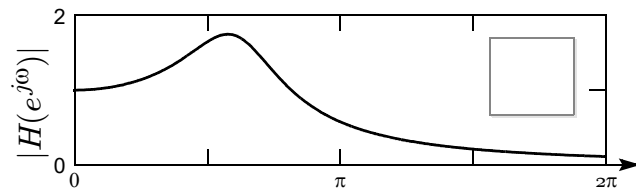
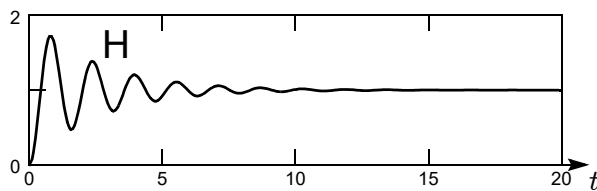
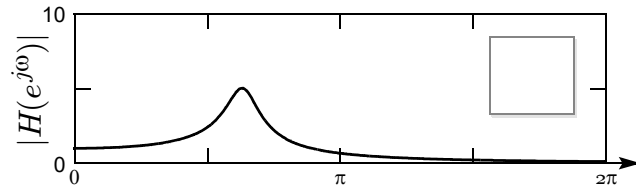
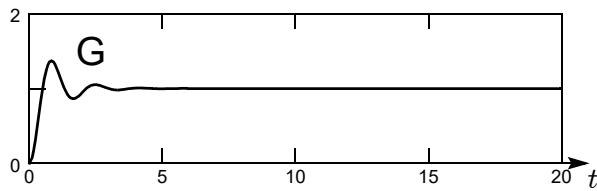
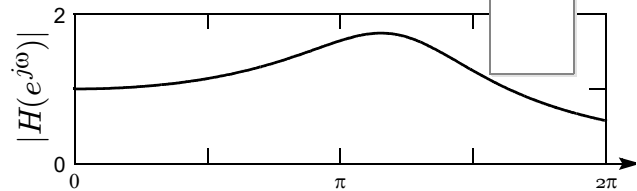
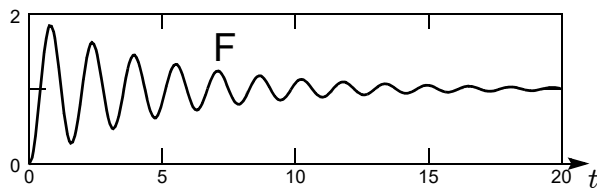
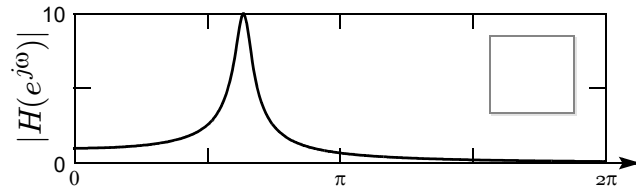
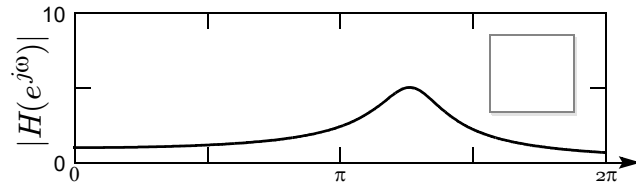
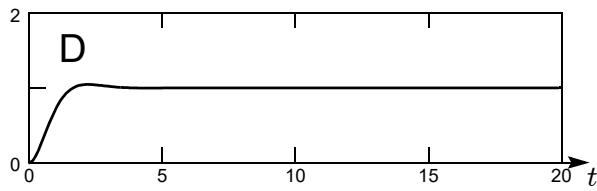
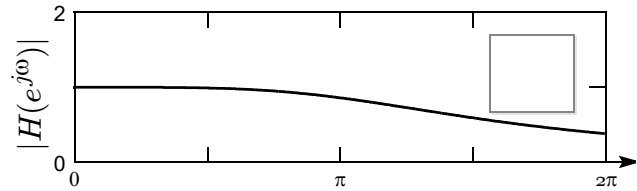
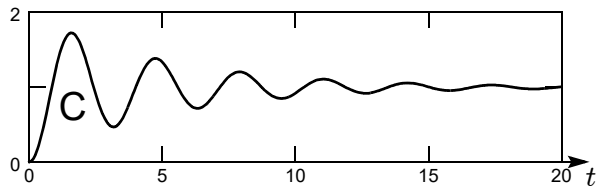
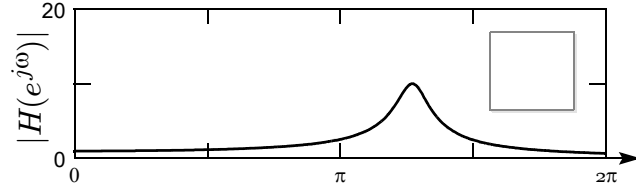
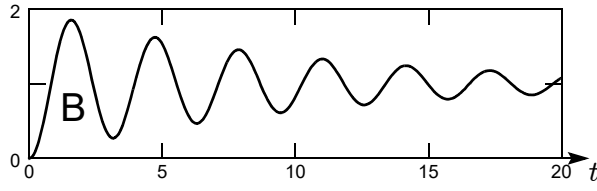
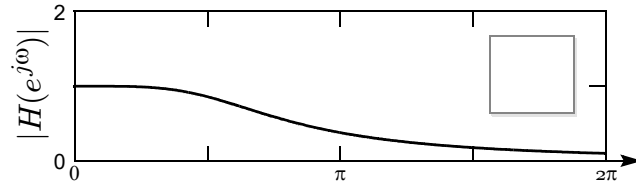
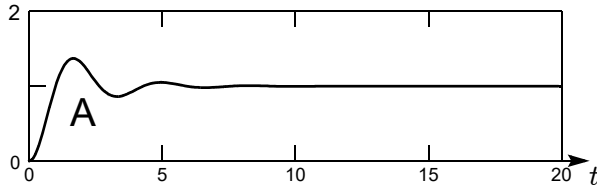






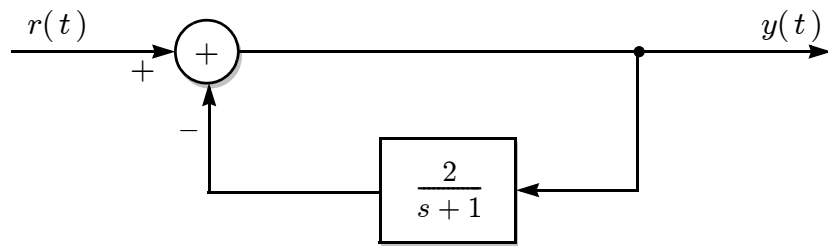


**PROBLEM 4.** Shown on the left are the step responses of eight second-order low-pass filters, labeled A through H. Shown on the right are the magnitude responses for these filters, but in a scrambled order. Match each magnitude response to its corresponding step response by writing a letter (A through H) in each answer box.



**PROBLEM 5.** (15 points)

Consider the following closed-loop system with zero initial conditions:



When the input is the decaying exponential  $r(t) = e^{-t}u(t)$ , the output can be written as:

$$y(t) = (Ae^{-t} + Be^{-Ct})u(t),$$

where

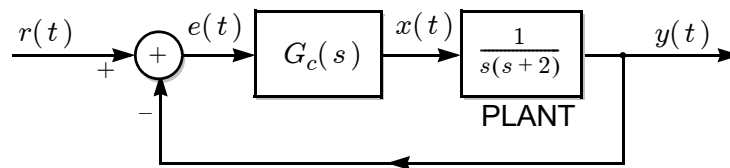
$$A = \boxed{\phantom{000}}$$

$$B = \boxed{\phantom{000}}$$

$$C = \boxed{\phantom{000}}.$$

**PROBLEM 6.** (20 points)

The diagram below shows feedback control of a plant with transfer function  $G_p(s) = \frac{1}{s(s+2)}$ :



The closed-loop transfer function is  $H(s) = Y(s)/R(s)$ . The controller can be expressed as:

$$G_c(s) = K_p + \frac{K_i}{s} + K_d s.$$

NOTATION:	$K_p$	$K_i$	$K_d$
P:	nonzero	0	0
PI:	nonzero	nonzero	0
PD:	nonzero	0	nonzero
PID:	nonzero	nonzero	nonzero

(a)  $H(s)$  is a *third-order* system when using [ P ] [ PI ] [ PD ] [ PID ] control. (Circle all that apply.)

(b)  $H(s)$  is a *second-order* system when using [ P ] [ PI ] [ PD ] [ PID ] control. (Circle all that apply.)

(c) The d.c. gain is  $H(0) = 1$  when using [ P ] [ PI ] [ PD ] [ PID ] control. (Circle all that apply.)

(d) With P control, oscillations in the closed-loop step response can be avoided by choosing  $K_p < \boxed{\phantom{0000}}$ .

(e) With P control, a damping ratio of  $\zeta = 1/\sqrt{2}$  can be achieved by choosing  $K_p = \boxed{\phantom{0000}}$ .

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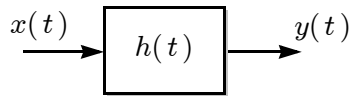
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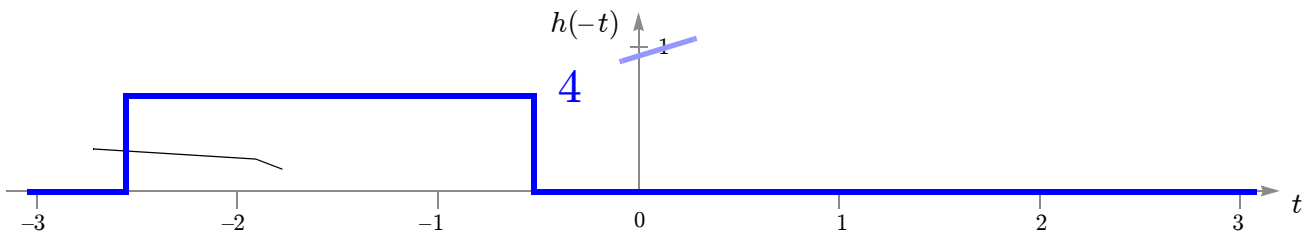
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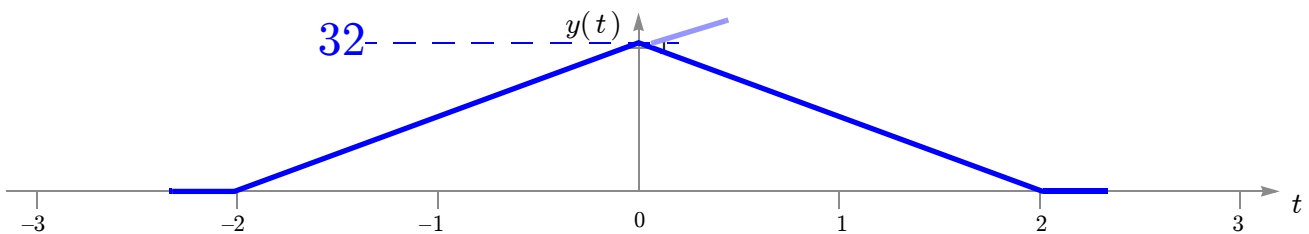
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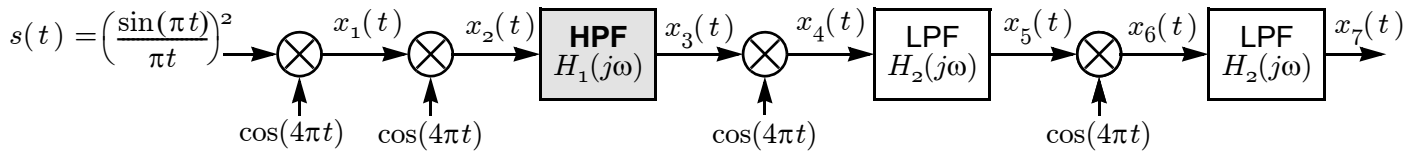
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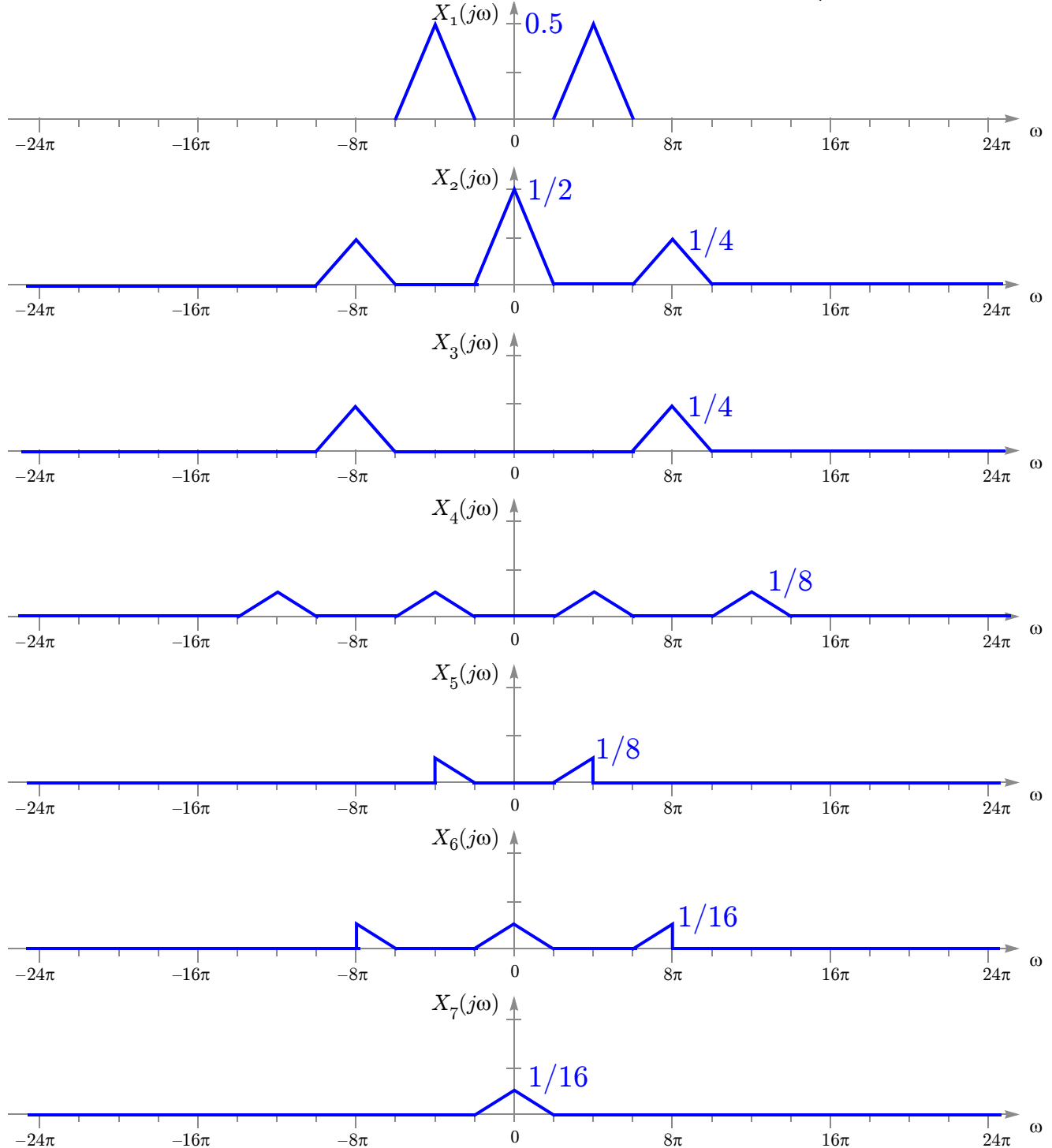
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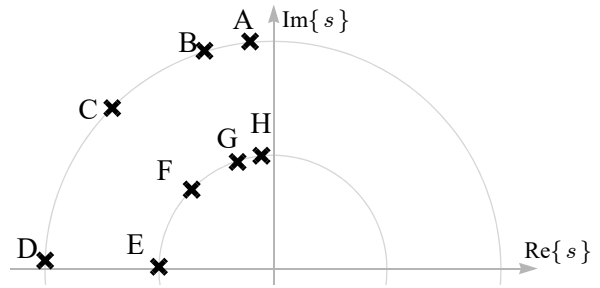
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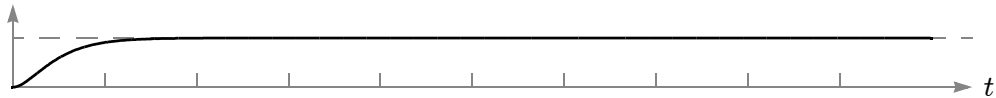
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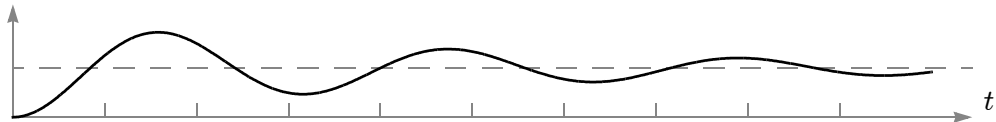
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(a) .

D



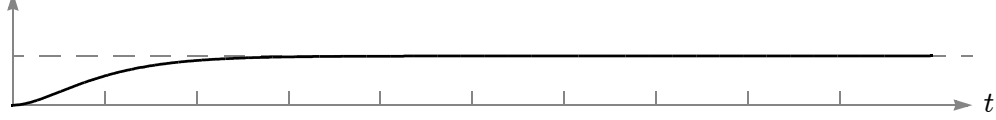
H



B



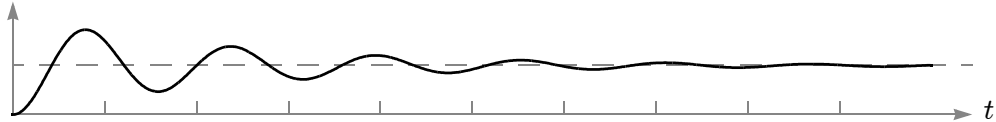
E



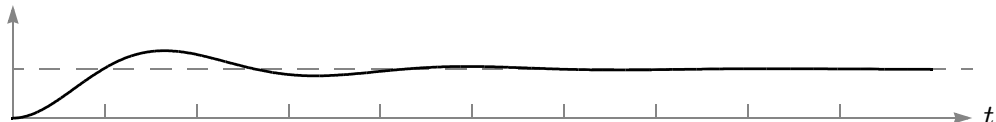
C



A



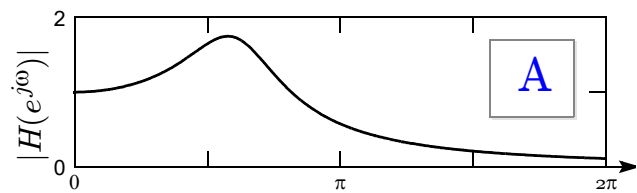
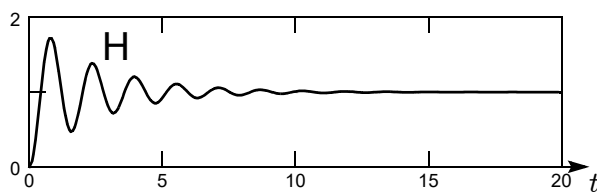
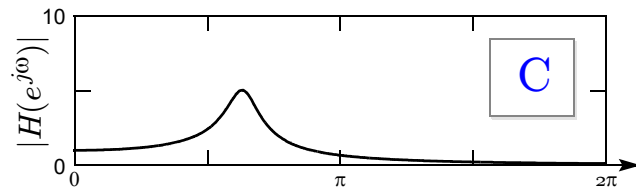
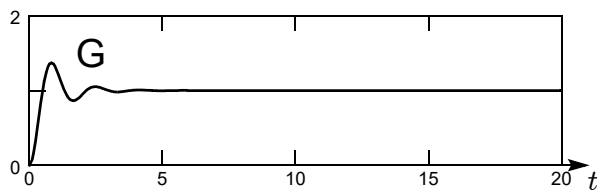
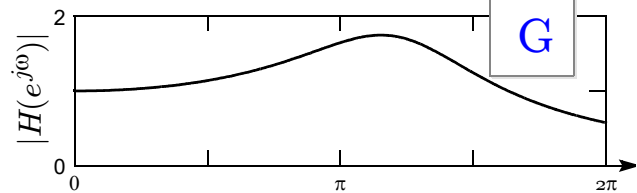
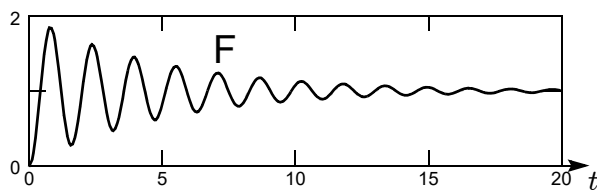
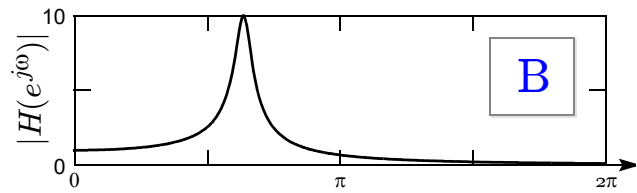
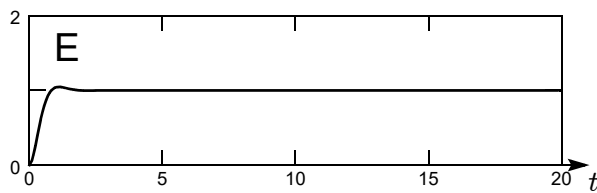
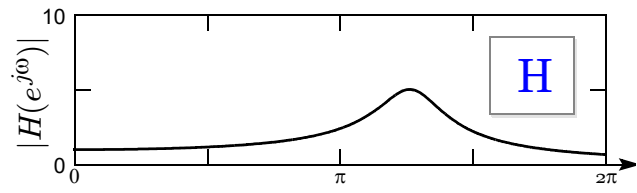
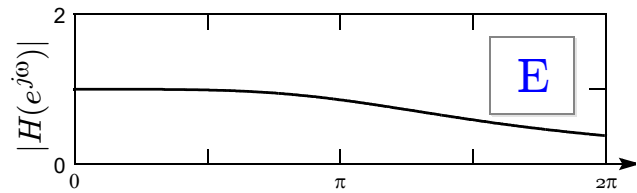
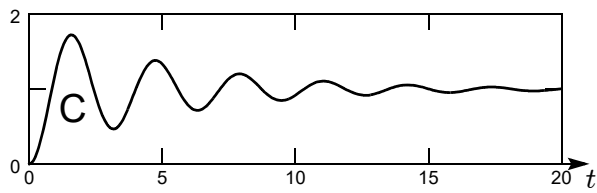
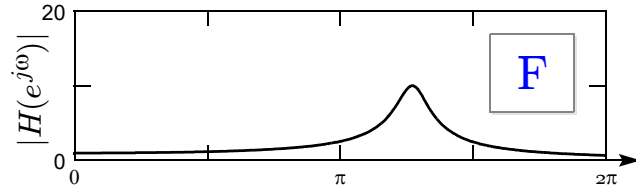
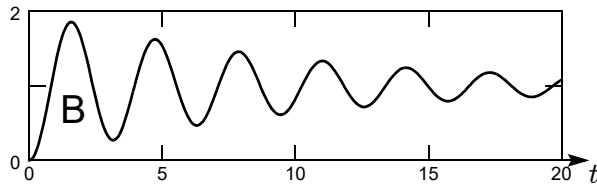
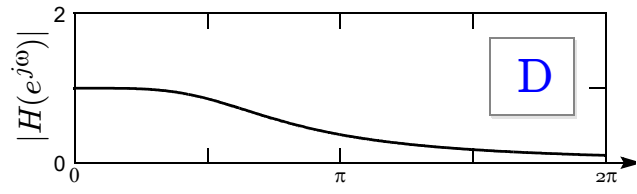
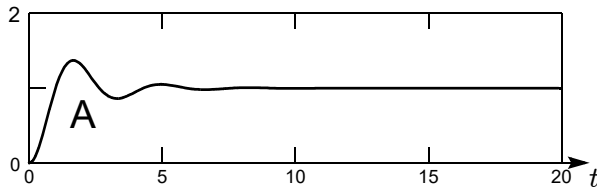
G



F

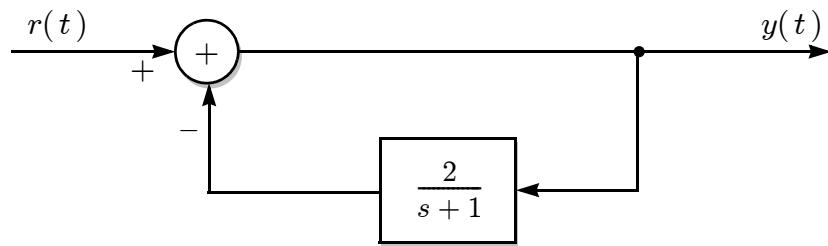


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**PROBLEM 5.** (15 points)

Consider the following closed-loop system with zero initial conditions:



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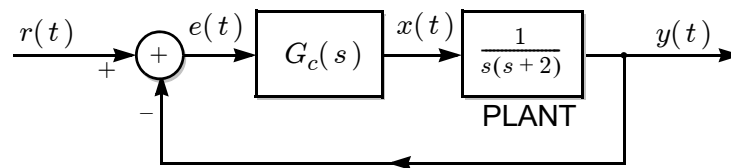
$$A = \boxed{0}$$

$$B = \boxed{1}$$

$$C = \boxed{3}$$

**PROBLEM 6.** (20 points)

The diagram below shows feedback control of a plant with transfer function  $G_p(s) = \frac{1}{s(s+2)}$ :



The closed-loop transfer function is  $H(s) = Y(s)/R(s)$ . The controller can be expressed as:

$$G_c(s) = K_p + \frac{K_i}{s} + K_d s.$$

NOTATION:	$K_p$	$K_i$	$K_d$
P:	nonzero	0	0
PI:	nonzero	nonzero	0
PD:	nonzero	0	nonzero
PID:	nonzero	nonzero	nonzero

(a)  $H(s)$  is a *third-order* system when using [ P ]  PI  PD  PID control. (Circle all that apply.)

(b)  $H(s)$  is a *second-order* system when using  P  PI  PD  PID control. (Circle all that apply.)

(c) The d.c. gain is  $H(0) = 1$  when using  P  PI  PD  PID control. (Circle all that apply.)

(d) With P control, oscillations in the closed-loop step response can be avoided by choosing  $K_p < \boxed{1}$ .

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